

# Capturing a Non-Cooperative Tumbling Object: A Control Barrier Function Approach

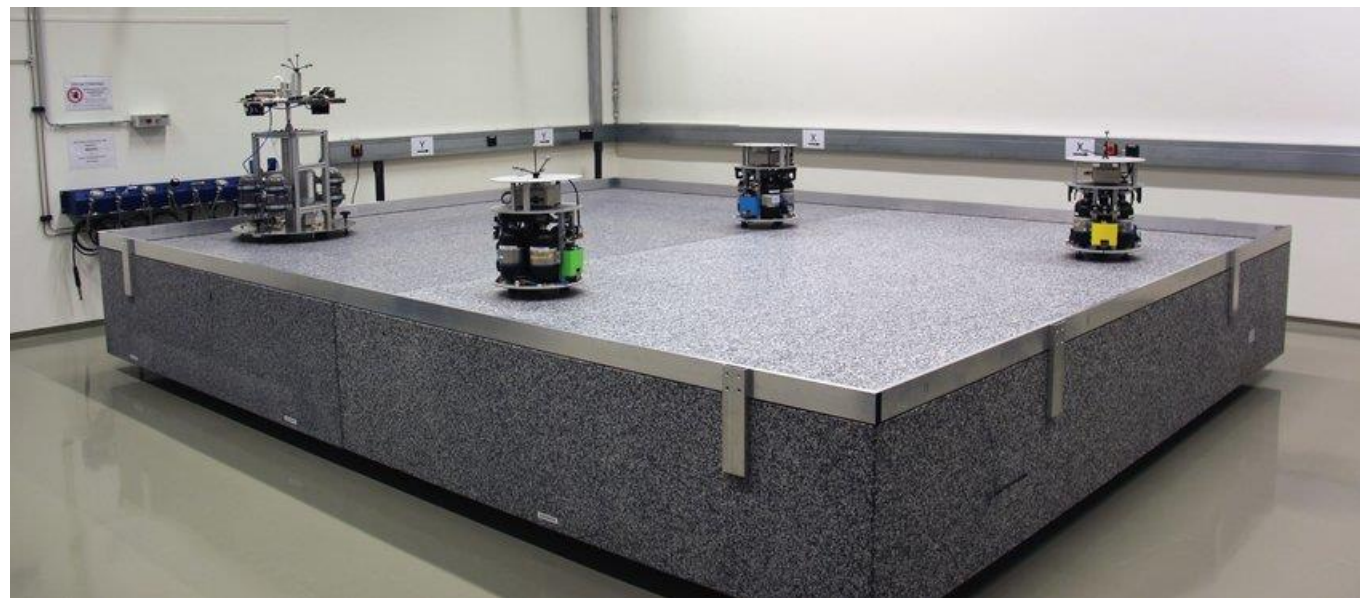


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# Problem Statement

- Summer Intern at RV as a SMART Scholar
- Assigned to work in the ROC lab
- Satellite capture problem
  - rescue, inspection, refueling, upgrades, etc

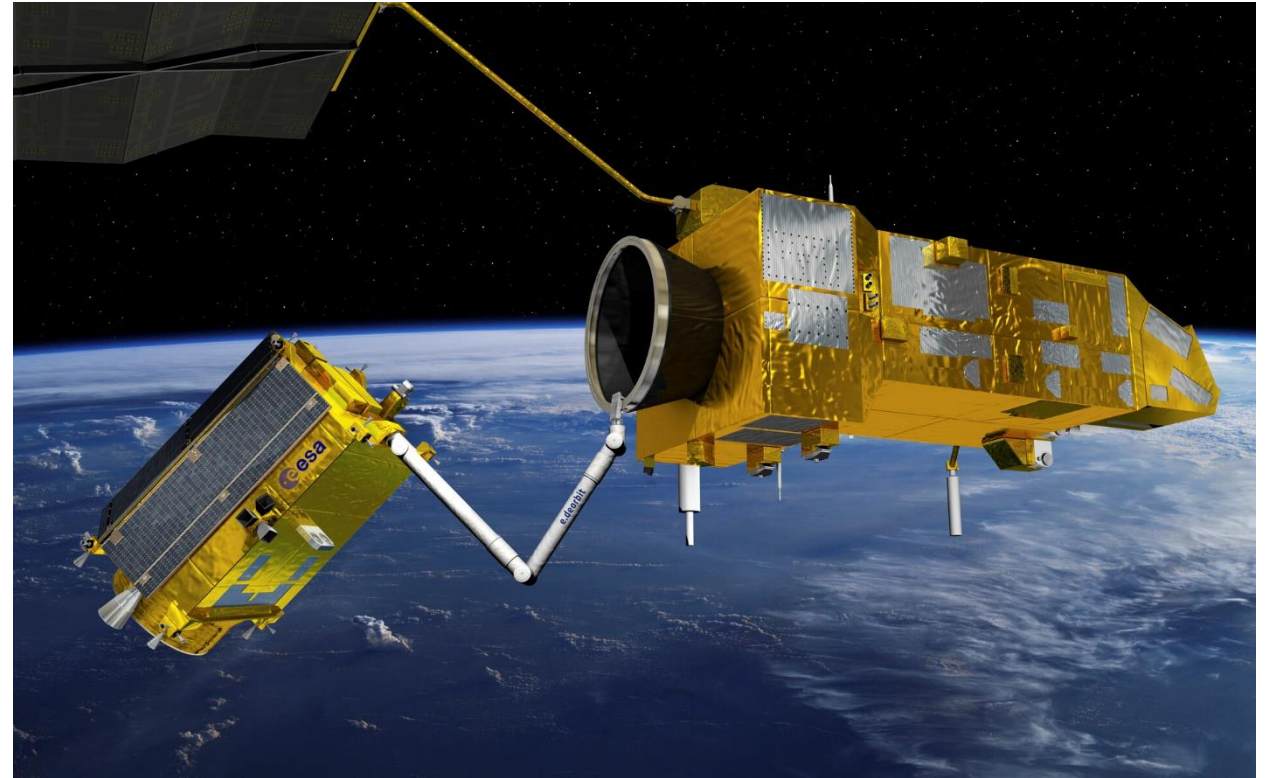


Daitx, Henrique (2015) *Development of a combined attitude and position controller for a satellite simulator*. Master's, Cranfield University, UK

# Problem Statement



- Non-cooperative (i.e., an unknown or tumbling object with a varying axis of rotation)
- Multiple redundant joint manipulators
- Safety Constraints
  - Collision avoidance Constraints
    - Client-Server
    - Manipulator-Server
    - Manipulator-Manipulator
  - Dynamic singularity avoidance Constraint
  - Vision constraints
    - Keep client agent in line of sight
    - Don't look at the sun (saved for future work)
- Robustness
  - Uncertain client agent dynamics
  - Disturbances and perturbations
- Energy Considerations
  - Free-Floating VS Free-Flying
- Computational efficiency, possibly real time implementation
  - Computational resource constraint



Rendering of the European Space Agency's proposed e.Deorbit mission for 2024  
[https://www.esa.int/ESA\\_Multimedia/Images/2017/01/e.Deorbit\\_s\\_robotic\\_arm](https://www.esa.int/ESA_Multimedia/Images/2017/01/e.Deorbit_s_robotic_arm)



## Server Agent:

$$H^{(1)}(\delta^{(1)}, \Theta)\ddot{q}^{(1)} + C^{(1)}(\delta^{(1)}, \dot{\delta}^{(1)}, \Theta, \dot{\Theta}) = Q$$

- $Q \triangleq J_Q u$  are the generalized forces, where  $u \triangleq [f, \tau, \tau_\theta]$ , and  $J_Q$  is a Jacobian
- $H^{(1)}$  is the known inertial matrix
- $C^{(1)}$  represents the known nonlinear terms
- $q^{(1)} \triangleq [r_{CM}^{(1)}, \delta^{(1)}, \Theta]$  is the generalized coordinate

## Client Agent:

$$H^{(2)}(X^{(2)})\ddot{X}^{(2)} + C^{(2)}(X^{(2)}, \dot{X}^{(2)}) + \tau_d(t) = 0$$

$$C^{(2)} \triangleq V(X^{(2)}, \dot{X}^{(2)}) + F_S(\dot{X}^{(2)}) + G(X^{(2)})$$

- The above terms are uncertain, but have known bounds
- $X^{(2)}$  and  $\dot{X}^{(2)}$  are measurable/calculable

## Control Affine Representation of the Whole System:

$$\dot{Z} \in F(Z, u),$$

$$F \triangleq \begin{bmatrix} z_2^{(1)} \\ z_2^{(2)} \\ -(H^{(1)})^{-1}C^{(1)} \\ -(H^{(2)})^{-1}(C^{(2)} + \bar{\tau}_d \mathbb{B}) \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ (H^{(1)})^{-1}Q \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

$$Z \triangleq [q^{(1)}, X^{(2)}, \dot{q}^{(1)}, \dot{X}^{(2)}, \text{mode}, W]$$



# Higher Order Control Barrier Function

- Use Higher Order Control Barrier Functions to act as a filter on the nominal controller.
- Constrained Quadratic Program
  - Constraints are inequalities
- Constraints are derived according to HOCBFs
- Find control input that is as close to the nominal controller that satisfies the constraints
- Should get us a real time controller that drives the server agent to the desired capture state while satisfying safety constraints.

$$Q^*(Z) = \underset{Q \in \mathbb{R}^N}{\operatorname{argmin}} \|Q - Q_{nom}\|^2$$

s. t.  $Q \in \mathbf{K}_0$  if mode = 0  
 $Q \in \mathbf{K}_1$  if mode = 1  
 $Q \in \mathbf{K}_2$  if mode = 2

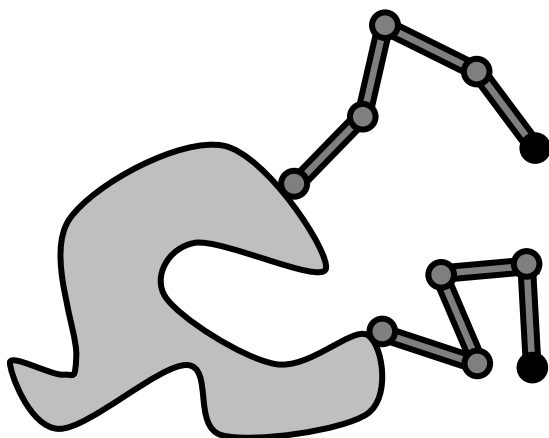
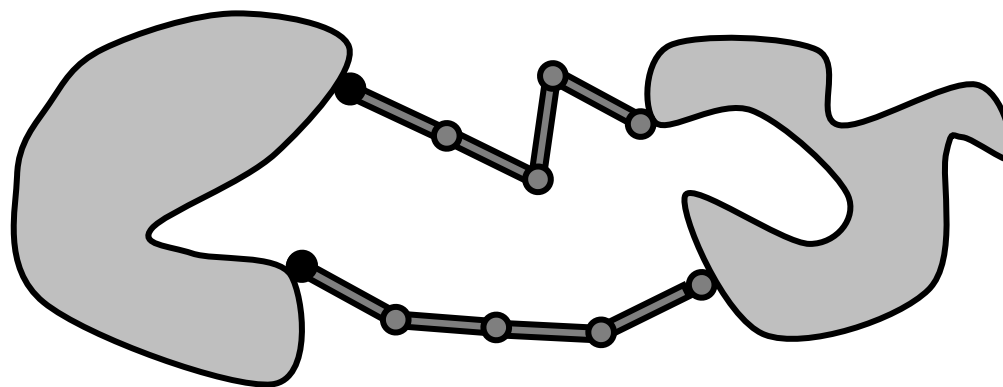
$$\|P_{1-3}Q\|^2 \leq f_{\max}^2$$
$$\|P_{4-6}Q\|^2 \leq \tau_{\max}^2$$
$$|P_{7-K}Q|^2 \leq \tau_{\theta, \max}^2$$





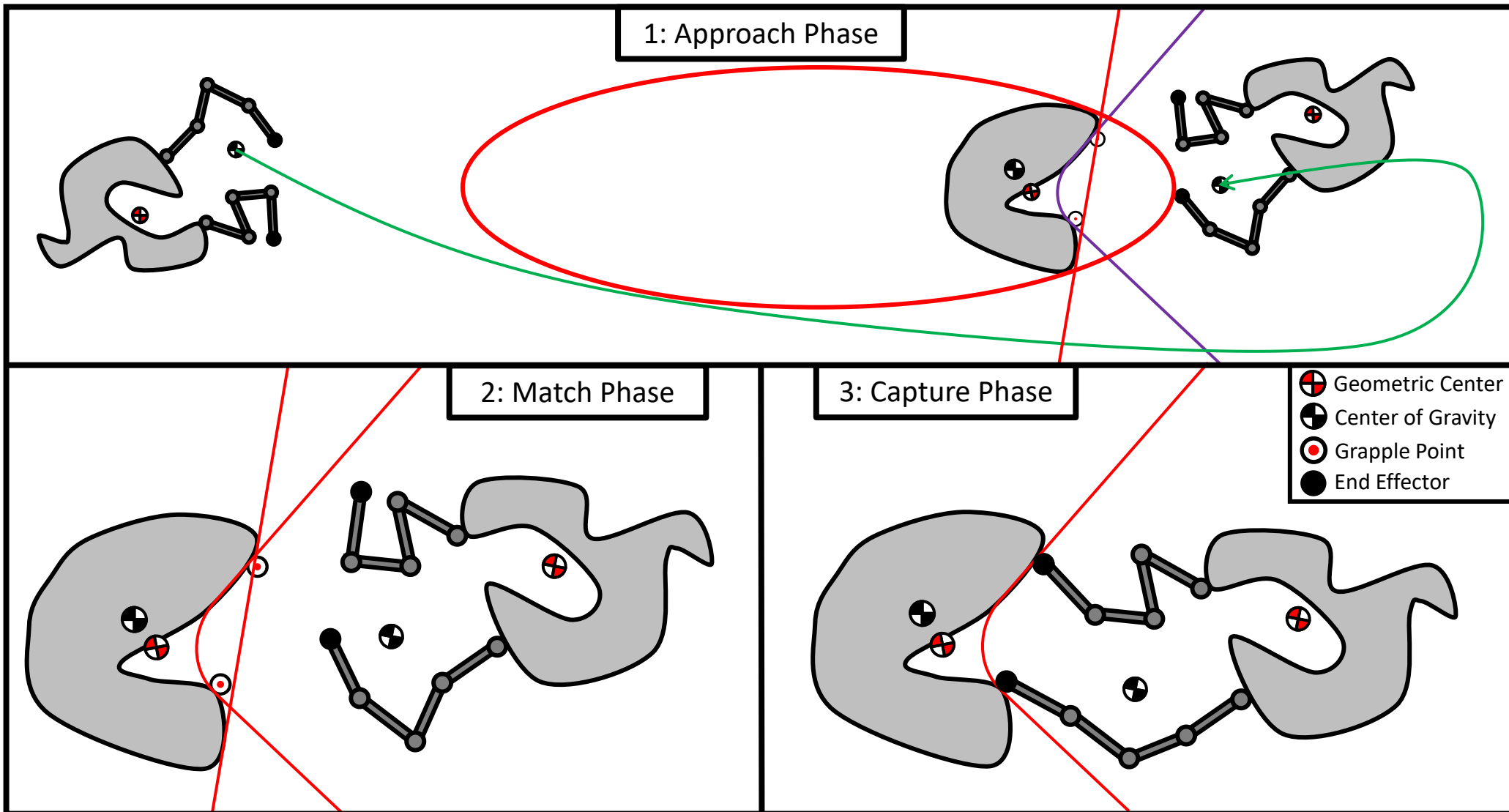
# Nominal Controller

- There is a nominal controller that is designed to stabilize to a desired final state (i.e., capture)
- Does not care about safety



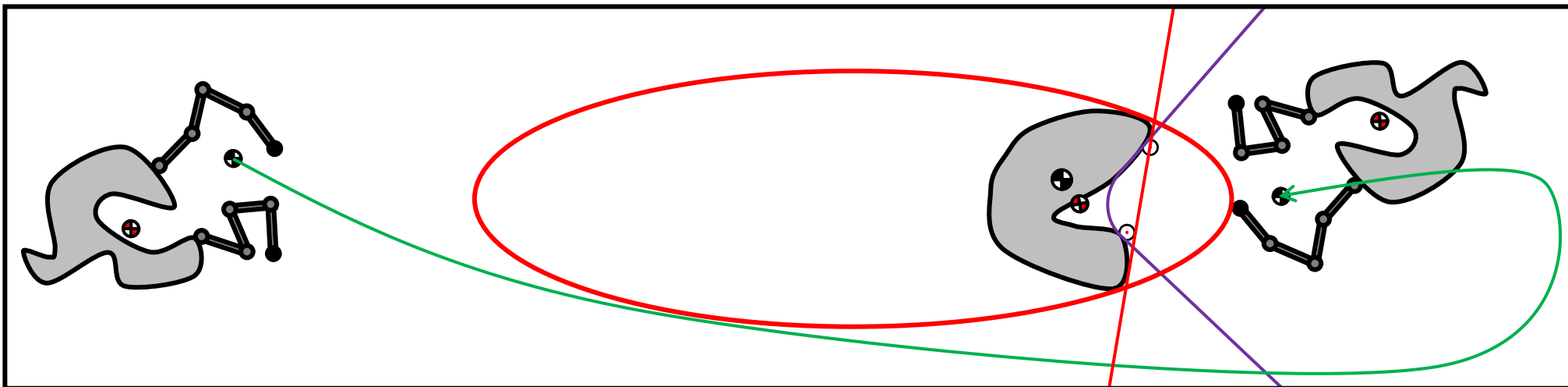


# Proposed Strategy (Operating Modes)





# Approach Phase: mode = 0



- Ellipsoid is fixed to the client agent, and is not only selected to prevent collisions, but also for trajectory shaping.
- Nominal controller will drive the server agent into the approach region (right of the purple surface)
  - This surface is fixed to the client agent.
- Server Agent is modelled as either a polyhedral, or a sphere

$$B_1 = \begin{cases} c - r_{GC}^{(1)}, & l = 0 \wedge m = 0 \\ \rho(\theta, \phi) - r_{GC}^{(1)}, & o/w \end{cases}$$

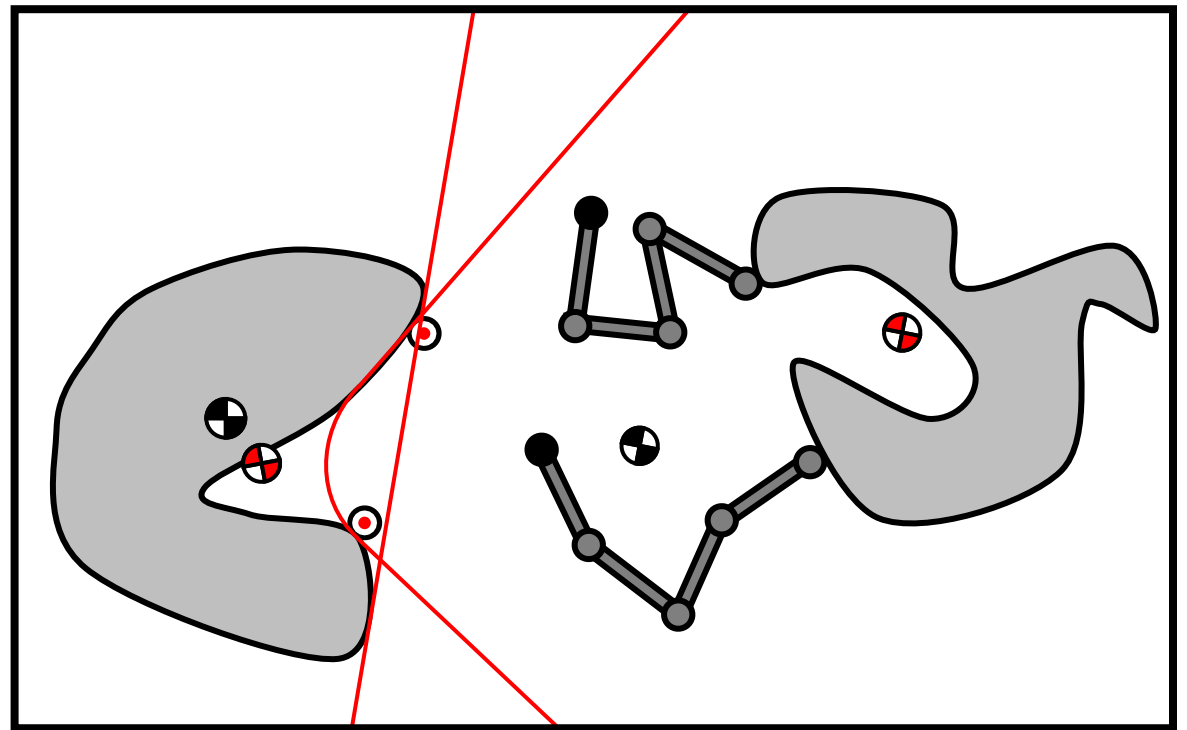
- The control input does not show up, so a recursion of the CBF candidate above is required:
- $\tilde{B}_1 = \Gamma_1 + \gamma_1 + \epsilon_1$
- The uncertain dynamics of the client agent show up, so the regulation map is:
- $\bar{K}_1 = \{Q \in \mathbb{R}^{6+K} : \bar{\Gamma}_1(Z, Q) \leq -\tilde{\gamma}_1(Z)\}$





# Match Phase: mode = 1

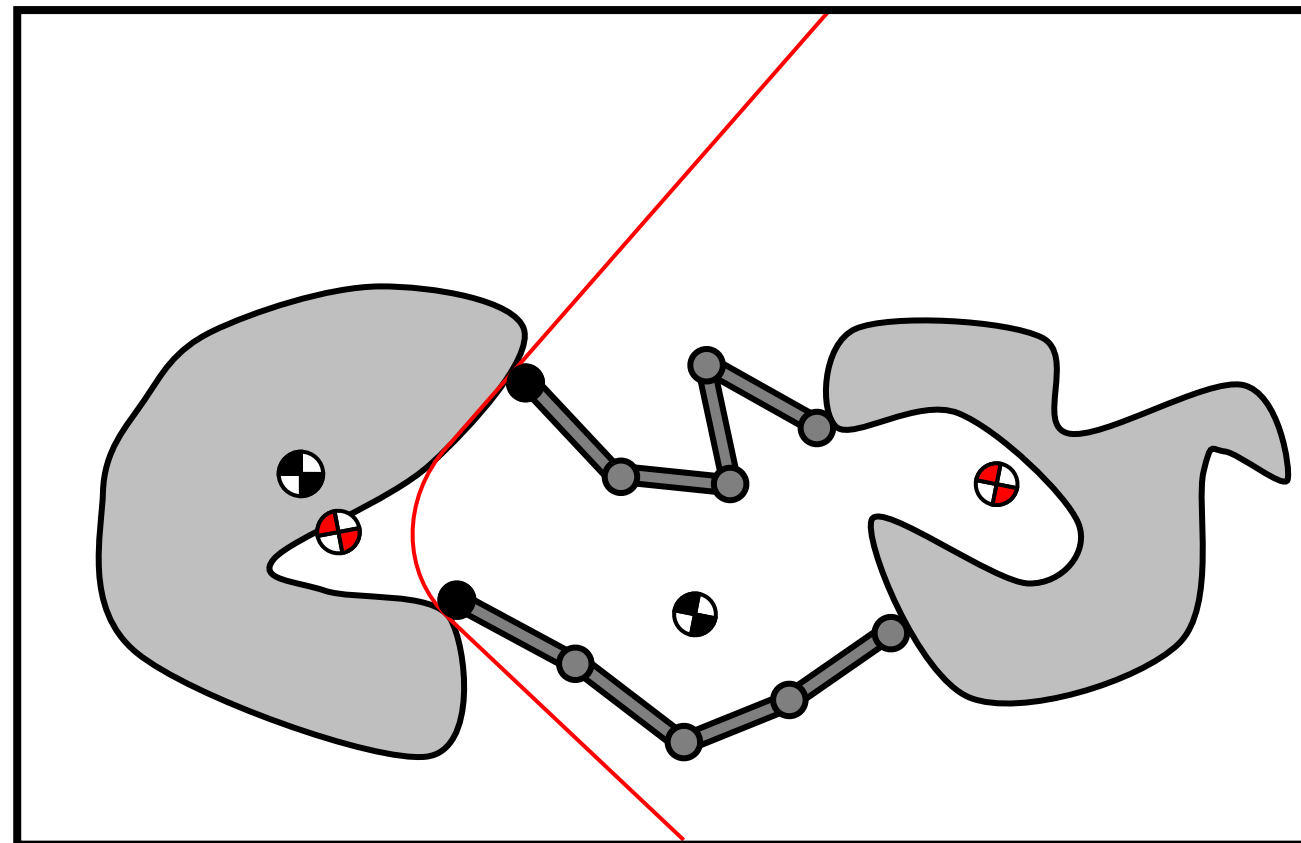
- Once the server agent falls into the approach region, a mode transition occurs, which erects a new safe set, which is better suited for this phase's goals.
- This phase allow for the relative velocities to regulate below a user specified threshold, thus setting the agent up for a safe capture in the next phase.
- The approach region and velocity matching barrier are promoted to CBF candidates.
- Like before, these CBF candidates have degree separation of two with the control input, and involves client agent uncertainties.





# Capture Phase: mode = 2

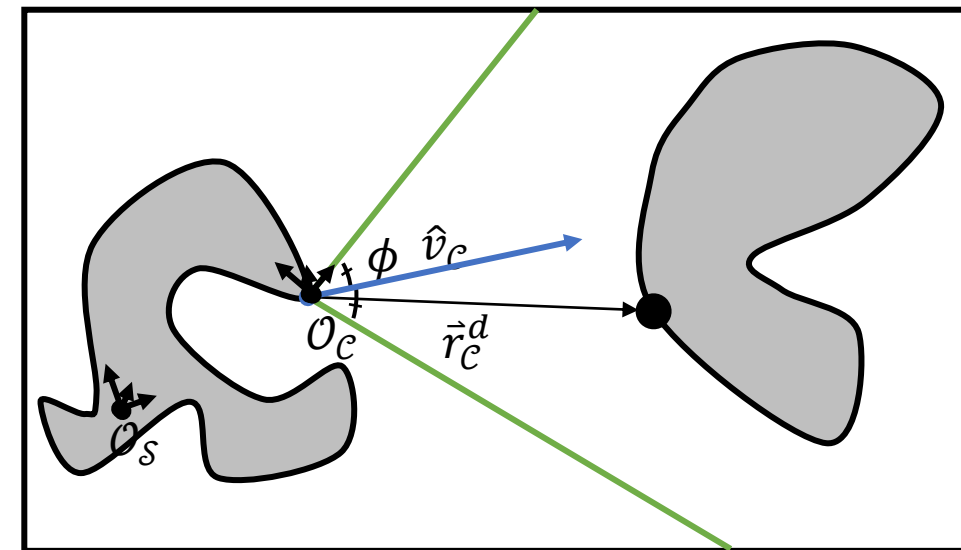
- Once the velocities are matched, the next mode transition occurs.
- In this phase, the velocity matching barrier is dropped, thus allowing the server agent to reach out and capture the client agent.
- In this situation, it may be desirable to have your control effort directed towards the manipulators, rather than the base:
  - Weighted pseudo-inverse of the server agent's Jacobian
  - $J_S^+ \triangleq W^{-1} J_S^T (J_S W^{-1} J_S^T)^{-1}$
  - $W$  is a user selected weight matrix





# General System Constraints

- These constraints are present during all the mission phases.
- Base Actuation Constraints
  - There is a maximum thrust and torque that can be applied to the server agent's base.
- Vision Constraint
  - Must keep the client agent within FoV of the server agent so to have state measurements of the client agent.
- Manipulator Actuation Constraints
  - There is a range of allowable joint angles for each joint
  - There is a maximum torque that each manipulator can have as an input
- Manipulator-Manipulator Collision Avoidance
  - With multiple manipulator arms, collision between them must be avoided
- Manipulator-Base Collision Avoidance
  - The manipulators are not allowed to collide with the server's base
- Dynamic Singularity Avoidance
  - There are configurations the server agent can be, where certain movements are physically prohibited, and therefore must be avoided.
  - The manipulability index  $\mu \triangleq \sqrt{\det(J_S J_S^T)}$  is used as a constraint
    - When it is zero,  $J_S$  loses rank, and is full rank otherwise





- Each operating mode (or phase) has its own safe set, where each safe set is pre-asymptotically stable.
- We do not get asymptotic stability since the safe set is not compact due to how the approach region constraints are designed.
- However, the nominal controller does drive the system to a particular state, thus, in practice, prohibiting the system from flowing without bound.
- It remains to be shown that this controller will operate in real time on a Raspberry Pi, but based on CBF based QP controllers being implemented on other systems using similar devices (e.g., Ames's group with the BeagleBone Black), it seems plausible.

$$Q^*(Z) = \underset{Q \in \mathbb{R}^N}{\operatorname{argmin}} \|Q - Q_{nom}\|^2$$

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 $|P_{7-K}Q| \leq \tau_{\theta, \max}$



- Simulations
- Conduct experiments in the ROC lab
- Multiple Impedance Controller as the nominal controller
- Investigate the “don’t look at the sun” constraint

