

Comments on “Adaptive Variable Structure Set-Point Control of Underactuated Robots”

W. E. Dixon and E. Zergeroglu

Recently, an adaptive variable structure controller was proposed in the above note¹ to solve the set-point problem for underactuated robots. Specifically, a time-varying gain, denoted by $k(t) \in \mathbb{R}$, was utilized in the control development and stability analysis which was generated via a discontinuous differential equation. Unfortunately, due to the discontinuous nature of the time derivative of $k(t)$, erroneous arguments were utilized in the stability analysis which yield unexpected stability results.

To illustrate that the stability arguments are invalid, we propose the following counter example

$$\begin{aligned} \dot{x}_1(t) &= x_1(t) \\ \dot{x}_2(t) &= u_a(t) \end{aligned} \quad (1)$$

where $x_1(t), x_2(t) \in \mathbb{R}$ are states of the system, and $u_a(t) \in \mathbb{R}$ represents the control input. It is clear from (1) that $x_1(t)$ is *uncontrollable* and *unstable*. Based on the controller developed in the note,¹ the control input for the above system can be designed as follows:

$$u_a = -k_a x_2 - u_c \quad (2)$$

where the auxiliary control input, denoted by $u_c(t) \in \mathbb{R}$, is designed as follows:

$$u_c = \frac{(1+k)x_2}{x_2^2 + \delta} (k_u + 1)x_1^2 \quad (3)$$

where $k(t) \in \mathbb{R}$ is a positive, time-varying control gain that is generated via the following discontinuous differential equation:

$$\dot{k} = \begin{cases} \frac{\eta}{k} \left(\frac{kx_2^2 - \delta_1}{x_2^2 + \delta} \right) (k_u + 1)x_1^2, & \text{if } k \neq 0 \\ \delta, & \text{if } k = 0 \end{cases} \quad (4)$$

$k_a, k_u, \eta \in \mathbb{R}$ are positive, constant design parameters, and $\delta, \delta_1 \in \mathbb{R}$ are small positive constants, selected according to the following inequality:

$$\delta < \delta_1. \quad (5)$$

Based on the stability analysis presented in the note,¹ we define a nonnegative function, denoted by $V(t) \in \mathbb{R}$, to examine the stability of the system given in (1) as follows:

$$V = \frac{1}{2} x_1^2 + \frac{1}{2} x_2^2 + \frac{1}{2} \frac{k^2}{\eta}. \quad (6)$$

Manuscript received November 29, 1999; revised March 23, 2000. Recommended by Associate Editor P. Tomei.

W. E. Dixon is with Oak Ridge National Laboratory, Oak Ridge, TN 37831 USA (e-mail: dixonwe@ornl.gov).

E. Zergeroglu is with Lucent Technologies, Sturbridge, MA 01566 USA.

Publisher Item Identifier S 0018-9286(01)04144-7.

¹C.-Y. Su and Y. Stepanenko, *IEEE Trans. Automat. Contr.*, Vol. 44, pp. 2090–2093, Nov. 1999.

After taking the time derivative of (6) and substituting (1) for $x_1(t)$ and $x_2(t)$, we obtain the following expression:

$$\dot{V} = x_1^2 + x_2 u_a + \frac{k\dot{k}}{\eta}. \quad (7)$$

Then, we can substitute (2) for $u_a(t)$ and add/subtract the product $k_u x_1^2$ to the right side of (7) to conclude that

$$\dot{V} = -k_u x_1^2 - k_a x_2^2 - x_2 u_c + \frac{k\dot{k}}{\eta} + (k_u + 1)x_1^2. \quad (8)$$

After substituting (3) and (4) into (8) for $u_c(t)$ and $\dot{k}(t)$, respectively, and cancelling common terms, we have

$$\dot{V} = -k_u x_1^2 - k_a x_2^2 + \frac{1}{x_2^2 + \delta} (\delta - \delta_1)(k_u + 1)x_1^2, \quad \text{for } k \neq 0. \quad (9)$$

Based on (5), it is clear that

$$\dot{V} \leq -k_u x_1^2 - k_a x_2^2 \leq 0, \quad \text{for } k \neq 0 \quad (10)$$

hence, $x_1(t), x_2(t) \in \mathcal{L}_2$. Furthermore, since standard signal chasing arguments can be utilized to prove that $\dot{x}_1(t), \dot{x}_2(t) \in \mathcal{L}_\infty$ (which is a sufficient condition for $x_1(t), x_2(t)$ to be uniformly continuous), we can use Barbalat's Lemma to prove that

$$\lim_{t \rightarrow \infty} x_1(t), x_2(t) = 0. \quad (11)$$

From (1), it is obvious that the result given in (11) is impossible since $x_1(t)$ is *uncontrollable* and *unstable*. Note that the stability analysis presented in the note¹ does not examine the case when $k(t) = 0$, and, hence, it is not clear if the result given in the note¹ is valid for this case. Thus, based on this counter example, it appears that the piecewise continuous nature of the control development and stability analysis presented in the note¹ is erroneous.

Author's Reply

Chun-Yi Su

We would like to thank Dr. De Luca and Dr. Oriolo, Dr. Zhang, and Dr. Dixon and Dr. Zergeroglu for their inputs and interest with regards to the above note.¹ Through the use of counter-examples, they came across demonstrated results, which differed from those expected.

From the comments, we feel that there are important issues that were not duly emphasized in our note.

- 3) The constrained condition on the unactuated dynamic equation (3). The basic requirement is that the constrained equation (3) must be nonintegrable. If this is not the case, the second-order

Manuscript received November 6, 2000; revised November 29, 2000. Recommended by Associate Editor P. Tomei.

The author is with the Department of Mechanical Engineering, Concordia University, Montreal, PQ H3G 1M8, Canada (e-mail: cysu@me.concordia.ca). Publisher Item Identifier S 0018-9286(01)04143-5.

¹C.-Y. Su and Y. Stepanenko, *IEEE Trans. Automat. Contr.*, Vol. 44, pp. 2090–2093, Nov. 1999.